

Tutorial 8

Flow measurement

1. A jet of water issuing from 5mm diameter orifice working under a head of 2.0m, was found to travel horizontal and vertical distances of 2.772m and 1m respectively. If $C_c = 0.61$, determine discharge.

Solution:

Diameter of jet (d) = 5mm = 0.005m

C/s of jet (a) = $\frac{\pi}{4} \times 0.005^2 = 1.96 \times 10^{-5} \text{ m}^2$

Head (H) = 2m

x = 2.772m, y = 1m

$C_c = 0.61$

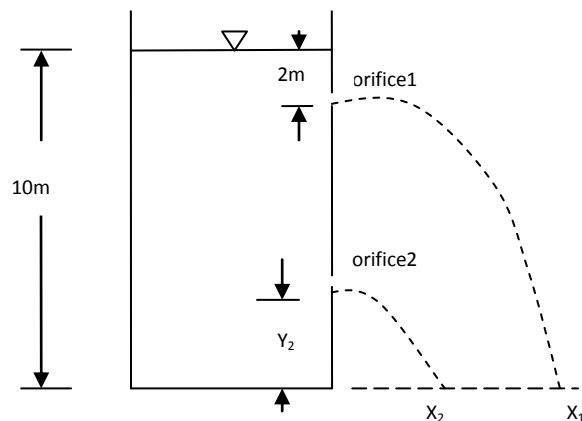
Discharge (Q) = ?

$$C_v = \frac{x}{\sqrt{4yH}} = \frac{2.772}{\sqrt{4 \times 1 \times 2}} = 0.98$$

$$C_d = C_c C_v = 0.61 \times 0.98 = 0.5978$$

$$Q = C_d a \sqrt{2gH} = 0.5978 \times 1.96 \times 10^{-5} \sqrt{2 \times 9.81 \times 2} = 7.34 \times 10^{-5} \text{ m}^3/\text{s} = 0.0734 \text{ lps}$$

2. For the two orifices shown in the figure below, determine Y_2 such that $X_2 = \frac{3X_1}{4}$.



Solution:

$$H_1 = 2\text{m}, Y_1 = 10 - 2 = 8\text{m}, H_2 = 10 - Y_2$$

$$X_2 = \frac{3X_1}{4}$$

$Y_2 = ?$

$$\text{Coefficient of velocity for orifice 1 } (C_{v1}) = \frac{X_1}{\sqrt{4Y_1H_1}}$$

$$\text{Coefficient of velocity for orifice 2 } (C_{v2}) = \frac{X_2}{\sqrt{4Y_2H_2}}$$

Since the two orifices are identical

$$C_{v1} = C_{v2}$$

$$\frac{X_1}{\sqrt{4Y_1H_1}} = \frac{X_2}{\sqrt{4Y_2H_2}}$$

$$\frac{X_1^2}{4Y_1H_1} = \frac{X_2^2}{4Y_2H_2}$$

$$\frac{X_1^2}{4 \times 2 \times 8} = \frac{\left(\frac{3X_1}{4}\right)^2}{4Y_2(10-Y_2)}$$

$$Y_2^2 - 10Y_2 + 9 = 0$$

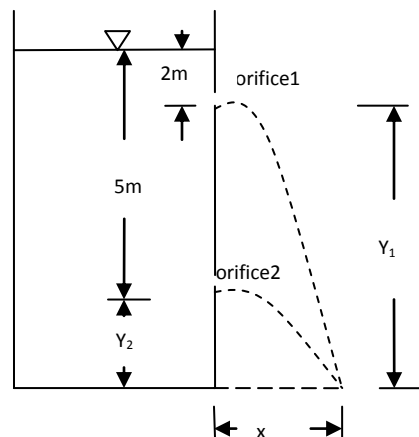
Solving for Y_2

$$Y_2 = 1, 9$$

As $Y_1 = 8\text{m}$, $Y_2 = 9 (>Y_1)$ is not feasible.

Hence $Y_2 = 1\text{m}$

3. A vessel has two identical orifices provided in one of its sides as shown in the figure. Locate the point of intersection of two jets. Take $C_v = 0.98$ for both orifices.



Solution:

$$C_v = \frac{x}{\sqrt{4yH}}$$

$$C_{v1} = C_{v2}$$

$$\frac{x}{\sqrt{4Y_1H_1}} = \frac{x}{\sqrt{4Y_2H_2}}$$

$$Y_1H_1 = Y_2H_2$$

$$Y_1 \times 2 = Y_2 \times 5$$

$$Y_1 = 2.5Y_2 \quad (\text{a})$$

Here,

$$Y_1 - Y_2 = H_1 - H_2 = 3$$

From a and b

$$Y_1 = 5\text{m}, Y_2 = 2\text{m}$$

$$x = C_v \sqrt{4Y_1 H_1} = 0.98 \sqrt{4 \times 5 \times 2} = 6.2 \text{ m}$$

4. A rectangular orifice 1.0m wide and 1.5m deep is discharging water from a vessel. The top edge of the orifice is 0.8m below the water surface in the vessel. Calculate the discharge through the orifice if $C_d = 0.6$. Also calculate the percentage error if the orifice is treated as a small orifice.

Solution:

Width of orifice (b) = 1m

Depth of orifice (d) = 1.5m

$H_1 = 0.8 \text{ m}$, $H_2 = H_1 + d = 0.8 + 1.5 = 2.3 \text{ m}$

$C_d = 0.6$

Discharge (Q) through large orifice = ?

error in discharge treating as small orifice = ?

$$Q = \frac{2}{3} C_d b \sqrt{2g} (H_2^{3/2} - H_1^{3/2})$$

$$= \frac{2}{3} \times 0.62 \times 1 \sqrt{2 \times 9.81} (2.3^{3/2} - 0.8^{3/2}) = 5.076 \text{ m}^3/\text{s}$$

For small orifice, $h = H_1 + d/2 = 0.8 + 1.5/2 = 1.55 \text{ m}$

Discharge (Q1) through small orifice (Q1) = $C_d a \sqrt{2gH}$

$$= 0.62 \times 1 \times 1.5 \sqrt{2 \times 9.81 \times 1.55} = 5.13 \text{ m}^3/\text{s}$$

$$\% \text{ error in measuring discharge} = \frac{5.13 - 5.076}{5.076} \times 100 = 1.06\%$$

5. A rectangular orifice of 1.5m wide and 1.2m deep is fitted in one side of a large tank. The water level on one side of the orifice is 2m above the top edge of the orifice, while on the other side of the orifice, the water level is 0.4m below its top edge. Calculate the discharge through the orifice if $C_d = 0.62$.

Solution:

Width of orifice (b) = 1.5m

Depth of orifice (d) = 1.2m

Height of water from top edge of orifice (H_1) = 2m

Difference of water level on both sides (H) = 2 + 0.4 = 2.4m

Height of water from bottom edge of orifice (H_2) = $H_1 + d = 2 + 1.2 = 3.2$

$C_d = 0.62$

Discharge through partially submerged orifice (Q) = ?

$$Q = \frac{2}{3} C_d b \sqrt{2g} (H^{3/2} - H_1^{3/2}) + C_d b (H_2 - H) \sqrt{2gH}$$

$$= \frac{2}{3} \times 0.62 \times 1.5 \sqrt{2 \times 9.81} (2.4^{3/2} - 2^{3/2}) + 0.62 \times 1.5 (3.2 - 2.4) \sqrt{2 \times 9.81 \times 2.4}$$

$$= 7.55 \text{ m}^3/\text{s}$$

6. A horizontal venturimeter in a water main has a 20cm diameter at one end and tapers to 10cm at its throat. A piezometer installed at the inlet reads 30cm, while the one at the throat reads 18cm. Determine the discharge through the main, if $C_d = 0.98$.

Solution:

Diameter at inlet (d_1) = 20cm = 0.2m

C/s area of inlet (A_1) = $\frac{\pi}{4} \times 0.2^2 = 0.0314\text{m}^2$

Diameter at throat (d_2) = 10cm = 0.1m

C/s area of throat (A_2) = $\frac{\pi}{4} \times 0.1^2 = 0.00785\text{m}^2$

Pressure head at inlet ($P_1/\rho g$) = 30cm = 0.3m

Pressure head at throat ($P_2/\rho g$) = 18cm = 0.18m

Head (h) = $\frac{P_1}{\rho g} - \frac{P_2}{\rho g} = 0.12\text{m}$

$C_d = 0.98$

Discharge (Q) = ?

$$Q = C_d \sqrt{2gh} \frac{A_1 A_2}{\sqrt{A_1^2 - A_2^2}}$$

$$= 0.98 \sqrt{2 \times 9.81 \times 0.12} \frac{0.0314 \times 0.00785}{\sqrt{0.0314^2 - 0.00785^2}}$$

$$= 0.0122 \text{ m}^3/\text{s}$$

7. A horizontal venturimeter is used to measure the flow of water in a 200mm diameter pipe. The throat diameter of the venturimeter is 80mm and the discharge coefficient is 0.85. If the pressure difference between the two measurement points is 10cm of mercury, calculate the average velocity in the pipe.

Solution:

Diameter at inlet (d_1) = 200mm = 0.2m

C/s area of inlet (A_1) = $\frac{\pi}{4} \times 0.2^2 = 0.0314\text{m}^2$

Diameter at throat (d_2) = 80mm = 0.08m

C/s area of throat (A_2) = $\frac{\pi}{4} \times 0.08^2 = 0.00503\text{m}^2$

Pressure difference ($P_1 - P_2$) = 10cm of Hg = $\gamma_{Hg} h = 13.6 \times 9810 \times 0.1 \text{ Pa}$

$Z_1 = Z_2$

Head (h) = $\frac{P_1 - P_2}{\gamma} = \frac{13.6 \times 9810 \times 0.1}{9810} = 1.36\text{m}$

$C_d = 0.85$

Average velocity in the pipe (V) = ?

$$Q = C_d \sqrt{2gh} \frac{A_1 A_2}{\sqrt{A_1^2 - A_2^2}}$$

$$= 0.85\sqrt{2 \times 9.81 \times 1.36} \frac{0.0314 \times 0.00503}{\sqrt{0.0314^2 - 0.00503^2}}$$

$$= 0.0223 \text{ m}^3/\text{s}$$

$$V = Q/A_1 = 0.0223/0.0314 = 0.71 \text{ m/s}$$

8. An orificemeter is provided in a vertical pipeline of 250mm diameter carrying oil of sp.gr. 0.9, the flow being upwards. The difference in elevation of the upstream and downstream ends of the manometer on the orificemeter is 350mm. The differential U-tube manometer shows a gauge deflection of 200mm. Calculate the discharge of oil. The diameter of the orifice is 150mm. Take $C_d = 0.65$.

Solution:

Diameter of pipe (d_1) = 250mm = 0.25m

C/s Area of pipe (A_1) = $\frac{\pi}{4} \times 0.25^2 = 0.049 \text{ m}^2$

Diameter of orifice (d_2) = 150mm = 0.15m

C/s Area of pipe (A_2) = $\frac{\pi}{4} \times 0.15^2 = 0.0176 \text{ m}^2$

Sp.gr. of oil (S_0) = 0.9

Difference in elevation ($Z_1 - Z_2$) = 350mm = 0.35m

Reading of manometer (x) = 200mm = 0.2m

Sp.gr. of mercury (S) = 13.6

$C_d = 0.65$

Discharge of oil (Q) = ?

Head h is given by

$$h = x \left(\frac{S}{S_0} - 1 \right) = 0.2 \left(\frac{13.6}{0.9} - 1 \right) = 2.82 \text{ m}$$

$$Q = C_d \sqrt{2gh} \frac{A_1 A_2}{\sqrt{A_1^2 - A_2^2}}$$

$$= 0.65 \sqrt{2 \times 9.81 \times 2.82} \frac{0.049 \times 0.0176}{\sqrt{0.049^2 - 0.0176^2}}$$

$$= 0.091 \text{ m}^3/\text{s}$$

9. A 20cmx10cm venturimeter is mounted in a vertical pipeline carrying oil of sp.gr. 0.8 flowing upwards. The throat section is 20cm above the entrance section of the venturimeter. The differential U-tube manometer shows a gauge deflection of 25cm. Calculate the discharge of the oil and the pressure difference between the entrance and the throat section. Take $C_d = 0.96$

Solution:

Diameter at inlet (d_1) = 20cm = 0.2m

C/s area of inlet (A_1) = $\frac{\pi}{4} \times 0.2^2 = 0.0314 \text{ m}^2$

Diameter at throat (d_2) = 10cm = 0.1m

C/s area of throat (A_2) = $\frac{\pi}{4} \times 0.1^2 = 0.00785 \text{ m}^2$

Sp.gr. of oil (S_0) = 0.8

Density of oil (ρ) = $0.8 \times 1000 = 800 \text{ kg/m}^3$

Difference in elevation ($Z_2 - Z_1$) = $20 \text{ cm} = 0.2 \text{ m}$

Reading of manometer (x) = $25 \text{ mm} = 0.025 \text{ m}$

Sp.gr. of mercury (S) = 13.6

Discharge of oil (Q) = ?

Pressure difference ($P_1 - P_2$) = ?

Head h is given by

$$h = x \left(\frac{S}{S_0} - 1 \right) = 0.025 \left(\frac{13.6}{0.8} - 1 \right) = 4 \text{ m}$$

$$Q = C_d \sqrt{2gh} \frac{A_1 A_2}{\sqrt{A_1^2 - A_2^2}}$$
$$= 0.96 \sqrt{2 \times 9.81 \times 4} \frac{0.0314 \times 0.00785}{\sqrt{0.0314^2 - 0.00785^2}}$$
$$= 0.0689 \text{ m}^3/\text{s}$$

h is also expressed as

$$h = \frac{P_1 - P_2}{\rho g} + (Z_1 - Z_2)$$

$$\frac{P_1 - P_2}{\rho g} = 4 + 0.2$$

$$P_1 - P_2 = 4.2 \times 800 \times 9.81 = 32962 \text{ N/m}^2$$

10. A venturimeter with a throat diameter of 100mm is fitted in a vertical pipeline of 200mm diameter with oil of sp.gr. 0.88 flowing upwards. The venturimeter coefficient is 0.98. The pressure gauges are fitted at tapping points, one at the throat and the other in the inlet pipe 320mm below the throat. The difference between two pressure gauge readings is 28 kN/m^2 . Working from Bernoulli's equation, determine (a) the volume rate of oil through the pipe, (b) the difference in level in the two limbs of mercury if it is connected to the tapping points and connecting pipes are filled with same oil.

Solution:

Diameter at inlet (d_1) = $20 \text{ cm} = 0.2 \text{ m}$

$$C/s \text{ area of inlet } (A_1) = \frac{\pi}{4} \times 0.2^2 = 0.0314 \text{ m}^2$$

Diameter at throat (d_2) = $10 \text{ cm} = 0.1 \text{ m}$

$$C/s \text{ area of throat } (A_2) = \frac{\pi}{4} \times 0.1^2 = 0.00785 \text{ m}^2$$

Sp.gr. of oil (S_0) = 0.88

Density of oil (ρ) = $0.88 \times 1000 = 880 \text{ kg/m}^3$

Difference in elevation ($Z_2 - Z_1$) = $320 \text{ cm} = 0.32 \text{ m}$

Difference in pressure ($P_1 - P_2$) = $28 \text{ kN/m}^2 = 28000 \text{ N/m}^2$

Sp.gr. of mercury (S) = 13.6

$$C_d = 0.98$$

Discharge of oil (Q) = ?

Manometer reading (x) = ?

a. Applying Bernoulli's equation between inlet (1) and throat (2)

$$\frac{P_1}{\rho g} + \frac{V_1^2}{2g} + Z_1 = \frac{P_2}{\rho g} + \frac{V_2^2}{2g} + Z_2$$

$$\frac{P_1 - P_2}{\rho g} + (Z_1 - Z_2) = \frac{V_2^2}{2g} - \frac{V_1^2}{2g}$$

$$\frac{28000}{880 \times 9.81} + (-0.32) = \frac{V_2^2}{2g} - \frac{V_1^2}{2g}$$

$$\frac{V_2^2}{2g} - \frac{V_1^2}{2g} = 2.92 \quad (a)$$

According to continuity equation

$$A_1 V_1 = A_2 V_2$$

$$V_2 = \frac{A_1 V_1}{A_2} = \frac{0.0314 V_1}{0.00785} = 4V_1 \quad (b)$$

Solving a and b

$$\frac{(4V_1)^2}{2g} - \frac{V_1^2}{2g} = 2.92$$

$$V_1 = 1.95 \text{ m/s}$$

$$\text{Discharge (Q)} = A_1 V_1 = 0.0314 \times 1.95 = 0.612 \text{ m}^3/\text{s}$$

$$\text{Actual discharge} = C_d Q = 0.98 \times 0.612 = 0.599 \text{ m}^3/\text{s}$$

$$b. h = \frac{P_1 - P_2}{\rho g} + (Z_1 - Z_2) = \frac{28000}{880 \times 9.81} + (-0.32) = 2.92$$

$$h = x \left(\frac{S}{S_0} - 1 \right)$$

$$2.92 = x \left(\frac{13.6}{0.88} - 1 \right)$$

$$x = 0.2 \text{ m}$$

11. A venturimeter is used for measurement of discharge of water in a horizontal pipeline. The ratio of the upstream pipe diameter and throat is 2:1 and upstream diameter is 300mm. Mercury manometer connected at the pipe and throat shows the reading of 0.24m and the loss of head through the meter is 1/8 of the throat velocity head. Calculate the discharge in the pipe using the continuity and energy equations.

Solution:

Pipe diameter (d_1): throat diameter (d_2) = 2:1

Pipe diameter (d_1) = 300mm = 0.3m

Throat diameter (d_2) = $d_1/2$ = 0.15m

$$C/s \text{ area of inlet } (A_1) = \frac{\pi}{4} \times 0.3^2 = 0.0707\text{m}^2$$

$$C/s \text{ area of throat } (A_2) = \frac{\pi}{4} \times 0.15^2 = 0.01767\text{m}^2$$

Manometer reading (x) = 0.24m

Sp.gr. of mercury (S) = 13.6

Velocity at inlet = V_1

Velocity at throat = V_2

$$\text{Head loss } (h_L) = \frac{1}{8} \cdot \frac{V_2^2}{2g}$$

Discharge in the pipe (Q) = ?

Head h is given by

$$h = x \left(\frac{S}{S_0} - 1 \right) = 0.24 \left(\frac{13.6}{1} - 1 \right) = 3.02\text{m}$$

Applying Bernoulli's equation between inlet (1) and throat (2)

$$\frac{P_1}{\rho g} + \frac{V_1^2}{2g} + Z_1 = \frac{P_2}{\rho g} + \frac{V_2^2}{2g} + Z_2 + h_L$$

$$\frac{P_1 - P_2}{\rho g} + (Z_1 - Z_2) = \frac{V_2^2}{2g} - \frac{V_1^2}{2g} + \frac{1}{8} \cdot \frac{V_2^2}{2g} \quad (a)$$

$$h = \frac{P_1 - P_2}{\rho g} + (Z_1 - Z_2) \quad (b)$$

From a and b

$$h = \frac{9V_2^2}{16g} - \frac{V_1^2}{2g}$$

$$\frac{9V_2^2}{16g} - \frac{V_1^2}{2g} = 3.02 \quad (c)$$

According to continuity equation

$$A_1 V_1 = A_2 V_2$$

$$V_2 = \frac{A_1 V_1}{A_2} = \frac{0.0707 V_1}{0.01767} = 4V_1 \quad (d)$$

Solving c and d

$$\frac{9(4V_1)^2}{16g} - \frac{V_1^2}{2g} = 3.02$$

$$V_1 = 1.86\text{m/s}$$

$$\text{Discharge } (Q) = A_1 V_1 = 0.0707 \times 1.86 = 0.131 \text{ m}^3/\text{s}$$

12. A horizontal venturimeter with inlet and throat diameters of 400mm and 200mm respectively, is connected to a pipe. If the pressure in the inlet portion is 200kPa and the vacuum pressure (negative) on the throat is 400mm of mercury, find the rate of flow in the pipe taking $C_d = 0.97$.

Solution:

Diameter at inlet (d_1) = 400mm = 0.4m

$$C/s \text{ area of inlet } (A_1) = \frac{\pi}{4} \times 0.4^2 = 0.1256\text{m}^2$$

Diameter at throat (d_2) = 200mm = 0.2m

C/s area of throat (A_2) = $\frac{\pi}{4} \times 0.2^2 = 0.0314\text{m}^2$

Pressure at inlet (P_1) = 200 Kpa = $200 \times 10^3 \text{N/m}^2$

Pressure head at throat = -400 mm of mercury

$C_d = 0.97$

Discharge (Q) = ?

Pressure head at inlet $\left(\frac{P_1}{\rho g}\right) = \frac{200000}{1000 \times 9.81} = 20.38\text{m}$ of water

Pressure head at throat $\left(\frac{P_2}{\rho g}\right) = -0.4 \text{ m of mercury} = -0.4 \times 13.6 \text{ m of water} = -5.44 \text{ m of water}$

$Z_1 = Z_2$

Head h is given as

$$h = \frac{P_1 - P_2}{\rho g} + (Z_1 - Z_2) = 20.38 - (-5.44) + 0 = 25.82\text{m}$$

$$Q = C_d \sqrt{2gh} \frac{A_1 A_2}{\sqrt{A_1^2 - A_2^2}}$$
$$= 0.97 \sqrt{2 \times 9.81 \times 25.82} \frac{0.1256 \times 0.0314}{\sqrt{0.1256^2 - 0.0314^2}}$$
$$= 0.708 \text{ m}^3/\text{s}$$

13. A Venturimeter is to be fitted in a horizontal pipe of 0.15m diameter to measure a flow of water which may be anything up to $240\text{m}^3/\text{hour}$. The pressure head at the inlet for this flow is 18m above atmospheric and the pressure head at the throat must not be lower than 7m below atmospheric. Between the inlet and the throat there is an estimated frictional loss of 10% of the difference in pressure head between these points. Calculate the minimum allowable diameter for the throat.

Solution:

Diameter of pipe (d_1) = 0.15m

C/s area of pipe (A_1) = $\frac{\pi}{4} \times 0.15^2 = 0.01767\text{m}^2$

Discharge (Q) = $240\text{m}^3/\text{hour} = \frac{240}{3600} = 0.0667\text{m}^3/\text{s}$

Velocity at inlet (V_1) = $Q/A_1 = 0.0667/0.01767 = 3.77\text{m/s}$

Pressure head at inlet $\left(\frac{P_1}{\rho g}\right) = 18\text{m}$

Pressure head at throat $\left(\frac{P_2}{\rho g}\right) = -7 \text{ m}$

$Z_1 = Z_2$

Head loss (h_L) = $0.1 \times \left(\frac{P_1}{\rho g} - \frac{P_2}{\rho g}\right) = 0.1(18+7) = 2.5\text{m}$

Diameter of throat (d_2) = ?

Applying Bernoulli's equation between inlet (1) and throat (2)

$$\frac{P_1}{\rho g} + \frac{V_1^2}{2g} + Z_1 = \frac{P_2}{\rho g} + \frac{V_2^2}{2g} + Z_2 + h_L$$

$$\frac{P_1}{\rho g} - \frac{P_2}{\rho g} = \frac{V_2^2}{2g} - \frac{V_1^2}{2g} + h_L$$

$$18 + 7 = \frac{V_2^2}{2g} - \frac{3.77^2}{2g} + 2.5$$

$$V_2 = 21.34 \text{ m/s}$$

$$C/S \text{ area of inlet } (A_2) = Q/V_2 = 0.0667/21.334 = 0.003126 \text{ m}^2$$

$$A_2 = \frac{\pi}{4} x d_2^2$$

$$0.003126 = \frac{\pi}{4} x d_2^2$$

$$d_2 = 0.063 \text{ m} = 63 \text{ mm}$$

14. A Venturimeter of throat diameter 0.07m is fitted in a 0.15m diameter vertical pipe in which liquid of relative density 0.8 flows downwards. Pressure gauges are fitted to the inlet and to the throat sections. The throat being 0.9m below the inlet. Taking the coefficient of the meter as 0.96 find the discharge a) when the pressure gauges read the same b) when the inlet gauge reads 15170 N/m² higher than the throat gauge.

Solution:

$$\text{Diameter of pipe } (d_1) = 0.15 \text{ m}$$

$$C/s \text{ area of pipe } (A_1) = \frac{\pi}{4} x 0.15^2 = 0.01767 \text{ m}^2$$

$$\text{Diameter at throat } (d_2) = 0.07 \text{ m}$$

$$C/s \text{ area of throat } (A_2) = \frac{\pi}{4} x 0.07^2 = 0.00385 \text{ m}^2$$

$$Z_1 - Z_2 = 0.9 \text{ m}$$

$$C_d = 0.96$$

$$\text{Discharge } (Q) = ?$$

$$\text{a) } P_1 = P_2$$

$$h = \frac{P_1 - P_2}{\rho g} + (Z_1 - Z_2) = 0 + 0.9 = 0.9 \text{ m}$$

$$Q = C_d \sqrt{2gh} \frac{A_1 A_2}{\sqrt{A_1^2 - A_2^2}}$$

$$= 0.96 \sqrt{2 \times 9.81 \times 0.9} \frac{0.01767 \times 0.00385}{\sqrt{0.01767^2 - 0.00385^2}}$$

$$= 0.016 \text{ m}^3/\text{s}$$

$$\text{b) } P_1 = P_2 + 15170$$

$$h = \frac{P_1 - P_2}{\rho g} + (Z_1 - Z_2) = \frac{15170}{0.8 \times 1000 \times 9.81} + 0.9 = 2.83 \text{ m}$$

$$Q = C_d \sqrt{2gh} \frac{A_1 A_2}{\sqrt{A_1^2 - A_2^2}}$$

$$= 0.96 \sqrt{2 \times 9.81 \times 2.83} \frac{0.01766 \times 0.00385}{\sqrt{0.01766^2 - 0.00385^2}}$$

$$= 0.0285 \text{ m}^3/\text{s}$$

15. Water is flowing over a sharp-crested rectangular weir of width 50cm into a tank with cross-sectional area 0.6m^2 . After a period of 30s the depth of water in the tank is 1.4m. Assuming a discharge coefficient of 0.9, determine the height of the water above the weir.

If the rectangular weir is replaced by a 90° notch weir with the same head and a discharge coefficient of 0.8, calculate the depth increase of the water in the tank after 30s.

Solution:

a) Width of rectangular weir (L) = 50cm = 0.5m

C/S area (A) = 0.6m^2

Depth of water in tank (h) = 1.4m

Volume of water in 30 Sec = Ah = $0.6 \times 1.4 = 0.84\text{m}^3$

Discharge (Q) = Volume/time = $0.84/30 = 0.028 \text{ m}^3/\text{s}$

$C_d = 0.9$

Height of water (H) = ?

$$Q = \frac{2}{3} C_d \sqrt{2g} L H^{3/2}$$

$$0.028 = \frac{2}{3} \times 0.9 \sqrt{2 \times 9.81} \times 0.5 \times H^{3/2}$$

$$H = 0.076\text{m}$$

b) With 90° V-notch, $C_d = 0.8$

Head (H) = 0.076m

Increase in depth after 30s (h_1) = ?

$$Q = \frac{8}{15} C_d \sqrt{2g} \tan(\theta/2) H^{5/2}$$

$$Q = \frac{8}{15} \times 0.8 \sqrt{2 \times 9.81} \tan(90/2) 0.076^{5/2} = 0.003 \text{ m}^3/\text{s}$$

$$Q = \frac{Ah_1}{t}$$

$$0.003 = \frac{0.6 \times h_1}{30}$$

$$h_1 = 0.15\text{m}$$

16. A sharp edged weir is to be constructed across a stream in which the normal flow is 200 litres/sec. If the maximum flow likely to occur in the stream is 5 times the normal flow then determine the length of weir necessary to limit the rise in water level to 40cm above that for normal flow. $C_d=0.61$.

Solution:

Normal discharge (Q_1) = 200 lps = $0.2 \text{ m}^3/\text{s}$

Maximum discharge (Q_2) = $5 \times 0.2 = 1 \text{ m}^3/\text{s}$

$C_d=0.61$

Water level for normal flow = y

For $y+0.4$, Length of weir (L) = ?

$$Q = \frac{2}{3} C_d \sqrt{2g} L H^{3/2}$$

$$Q_1 = \frac{2}{3} \times 0.61 \sqrt{2 \times 9.81} L y^{3/2}$$

$$0.2 = 1.801 L y^{3/2}$$

$$L = 0.111 y^{-3/2} \quad (\text{a})$$

$$Q_2 = \frac{2}{3} \times 0.61 \sqrt{2 \times 9.81} L (y + 0.4)^{3/2}$$

$$1 = 1.801 L (y + 0.4)^{3/2}$$

$$0.555 = L (y + 0.4)^{3/2} \quad (\text{b})$$

From a and b

$$0.555 = 0.111 y^{-3/2} (y + 0.4)^{3/2}$$

$$\frac{(y+0.4)^{3/2}}{y^{3/2}} = 5$$

$$\frac{y+0.4}{y} = 2.924$$

$$y = 0.208\text{m}$$

$$L = 0.111 y^{-3/2} = 0.111 \times 0.208^{-3/2} = 1.17\text{m}$$

17. Compute the flow rate if the measured head above the bottom of the V-notch is 35cm, when $\theta = 60^\circ$ and $C_d = 0.6$. If the flow is wanted within an accuracy of 2%, what are the limiting values of the head.

Solution:

$$\text{Head (H)} = 35\text{cm} = 0.35\text{m}$$

$$\theta = 45^\circ$$

$$C_d = 0.6$$

$$\text{Flow rate (Q)} = ?$$

$$Q = \frac{8}{15} C_d \sqrt{2g} \tan(\theta/2) H^{5/2}$$

$$Q = \frac{8}{15} \times 0.6 \sqrt{2 \times 9.81} \tan(60/2) H^{5/2} = 0.818 H^{5/2}$$

$$= 0.818 \times 0.35^{5/2} = 0.059 \text{ m}^3/\text{s}$$

With $\pm 2\%$ error

$$Q_1 = 0.059 + 0.02 \times 0.059 = 0.0602 \text{ m}^3/\text{s}$$

$$Q_2 = 0.059 - 0.02 \times 0.059 = 0.0578 \text{ m}^3/\text{s}$$

$$Q = 1.417 H^{5/2}$$

$$Q_1 = 1.417 H_1^{5/2}$$

$$0.0602 = 1.417 H_1^{5/2}$$

$$H_1 = 0.352 \text{ m}$$

$$Q_2 = 1.417H_2^{5/2}$$

$$0.0578 = 0.818H_2^{5/2}$$

$$H_2 = 0.346 \text{ m}$$

18. Water is flowing in a rectangular channel of 1m wide and 0.8m deep. Find the discharge over a rectangular weir of crest length 60cm if the head of water over the crest of weir is 30cm and water from channel flows over the weir. Take $C_d = 0.62$. Take velocity of approach into consideration.

Solution:

$$\text{Area of channel (A)} = 1 \times 0.8 = 0.8 \text{ m}^2$$

$$\text{Length of weir (L)} = 0.6 \text{ m}$$

$$\text{Head of water (H}_1\text{)} = 0.3 \text{ m}$$

$$C_d = 0.62$$

Discharge over a rectangular weir without velocity of approach is

$$Q = \frac{2}{3} C_d L \sqrt{2g} H_1^{3/2}$$

$$= \frac{2}{3} \times 0.62 \times 0.6 \sqrt{2 \times 9.81} \times 0.3^{3/2} = 0.18 \text{ m}^3/\text{s}$$

$$\text{Velocity of approach (V}_a\text{)} = Q/A = 0.18/0.8 = 0.225 \text{ m/s}$$

$$\text{Velocity head (h}_a\text{)} = \frac{V_a^2}{2g} = \frac{0.225^2}{2 \times 9.81} = 0.00258 \text{ m}$$

$$Q = \frac{2}{3} C_d L \sqrt{2g} [(H_1 + h_a)^{3/2} - h_a^{3/2}]$$

$$= \frac{2}{3} \times 0.62 \times 0.6 \sqrt{2 \times 9.81} [(0.3 + 0.00258)^{3/2} - 0.00258^{3/2}] = 0.183 \text{ m}^3/\text{s}$$

19. A broad-crested weir of length 40m, has 400mm height of water above its crest. Find the maximum discharge neglecting velocity of approach. If the velocity of approach is taken into consideration, find the maximum discharge when the channel has a cross-sectional area of 40m² on the upstream side. Take $C_d = 0.6$.

Solution:

$$\text{Length of weir (L)} = 40 \text{ m}$$

$$\text{Head of water (H}_1\text{)} = 0.4 \text{ m}$$

$$C_d = 0.6$$

Maximum discharge neglecting velocity of approach

$$Q_{max} = 1.705 C_d L H^{3/2}$$

$$= 1.705 \times 0.6 \times 40 \times 0.4^{3/2} = 10.352 \text{ m}^3/\text{s}$$

Taking velocity of approach into consideration

Area of channel (A) = 40 m²

Velocity of approach (V_a) = Q_{max}/A = 10.35/40 = 0.25875 m/s

Velocity head (h_a) = $\frac{V_a^2}{2g} = \frac{0.25875^2}{2 \times 9.81} = 0.0034\text{m}$

Maximum discharge considering velocity of approach

$$Q_{max} = 1.705C_d L [(H + h_a)^{3/2} - h_a^{3/2}]$$
$$= 1.705 \times 0.6 \times 40 [(0.4 + 0.0034)^{3/2} - 0.0034^{3/2}] = 10.476 \text{ m}^3/\text{s}$$

20. The heights of water on the upstream and downstream side of a submerged weir of length 3.5m are 300mm and 150mm respectively. If C_d for free and drowned portion is 0.6 and 0.8 respectively, find the discharge over the weir.

Solution:

Height of water on upstream side (H) = 0.3m

Height of water on downstream side (h) = 0.15m

Length of weir (L) = 3.5m

C_{d1} = 0.6, C_{d2} = 0.8

Discharge through drowned orifice (Q) = ?

$$Q = \frac{2}{3} C_{d1} L \sqrt{2g} (H - h)^{3/2} + C_{d2} L h \sqrt{2g(H - h)}$$
$$= \frac{2}{3} \times 0.6 \times 3.5 \sqrt{2 \times 9.81} (0.3 - 0.15)^{3/2} + 0.8 \times 3.5 \times 0.15 \sqrt{2 \times 9.81 (0.3 - 0.15)} = 1.08 \text{ m}^3/\text{s}$$

21. A 1.25m diameter circular tank contains water up to a height of 5m. At the bottom of the tank, an orifice of 50mm diameter is provided. Find the height of water above the orifice after 1.5 minutes. Take C_d = 0.62.

Solution:

Diameter of tank (D) = 1.25m

Area of tank (A) = $\frac{\pi}{4} \times 1.25^2 = 1.227 \text{ m}^2$

Diameter of orifice (d) = 50mm = 0.05m

Area of orifice (a) = $\frac{\pi}{4} \times 0.05^2 = 0.00196 \text{ m}^2$

Coeff. of discharge (C_d) = 0.62

Initial head (H₁) = 5m

Time (t) = 1.5 minutes = 90 Sec

Final head (H₂) = ?

From continuity

-Q dt = Adh

$$t = - \int_{H_1}^{H_2} \frac{A}{Q} dh$$

$$= - \int_{H_1}^{H_2} \frac{A}{C_d a_0 \sqrt{2gh}} dh$$

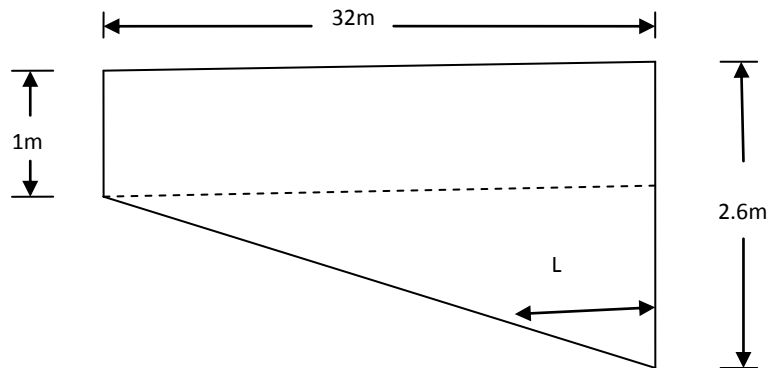
$$= \frac{2A(\sqrt{H_1} - \sqrt{H_2})}{C_d a_0 \sqrt{2g}}$$

$$90 = \frac{2 \times 1.227(\sqrt{5} - \sqrt{H_2})}{0.62 \times 0.00196 \sqrt{2 \times 9.81}}$$

$$0.197 = (2.236 - \sqrt{H_2})$$

$$H_2 = 4.15\text{m}$$

22. A rectangular swimming pool is 1m deep at one end and increases uniformly in depth to 2.6m at the other end. The pool is 8m wide and 32m long and is emptied through an orifice of area 0.224m^2 , at the lowest point in the side of the deep end. Taking C_d for the orifice as 0.6, find a) the time for the depth to fall by 1m b) the time to empty the pool completely.



Solution:

$$\text{Area of orifice } (a_0) = 0.224\text{m}^2$$

$$C_d = 0.6$$

a) For 1m fall in depth

$$H_1 = 2.6\text{m}, H_2 = 1.6\text{m}$$

Time to fall 1m depth (t_1) = ?

$$A = 32 \times 8 = 256\text{m}^2$$

From continuity

$$-Q dt = Adh$$

$$t_1 = - \int_{H_1}^{H_2} \frac{A}{Q} dh$$

$$= - \int_{H_1}^{H_2} \frac{A}{C_d a_0 \sqrt{2gh}} dh$$

$$= \frac{2A(\sqrt{H_1} - \sqrt{H_2})}{C_d a_0 \sqrt{2g}}$$

$$= \frac{2 \times 256 (\sqrt{2.6} - \sqrt{1.6})}{0.6 \times 0.224 \sqrt{2 \times 9.81}}$$

$$= 299 \text{ S}$$

b) Time to completely empty the tank (t) = ?

Let us find out the time to empty the tank (t₂) from H₁ = 1.6m to H₂ = 0m

We need A in terms of h.

$$A = 8L$$

$$\frac{L}{h} = \frac{32}{1.6}$$

$$L = 20h$$

$$A = 8 \times 20h = 160h$$

$$-Q dt = Adh$$

$$t_2 = - \int_{H_1}^{H_2} \frac{A}{Q} dh$$

$$= - \int_{H_1}^{H_2} \frac{160h}{C_d a_0 \sqrt{2gh}} dh = \frac{160}{C_d a_0 \sqrt{2g}} \int_{H_1}^{H_2} h^{1/2} dh$$

$$= \frac{160}{0.6 \times 0.224 \sqrt{2 \times 9.81}} \times \frac{2}{3} (H_1^{3/2} - H_2^{3/2})$$

$$= 179.2 (1.6^{3/2} - 0) = 363 \text{ S}$$

Time to completely empty the tank (t₁) = t₁ + t₂ = 299 + 363 = 662S

23. A cylindrical tank of internal diameter 0.6m, length 1.5m and axis vertical has a 5cm diameter sharp-edged orifice (C_d = 0.6) in the bottom, open to atmosphere. The tank is open at the top and empty. If water were admitted into the tank from above at a constant rate of 14lps, how long will it take to just fill the tank? How much water will escape through the orifice during that period?

Solution:

Diameter of tank (D) = 0.6m

$$\text{Area of tank (A)} = \frac{\pi}{4} \times 0.6^2 = 0.2827 \text{ m}^2$$

Diameter of orifice (d) = 5cm = 0.05m

$$\text{Area of orifice (a)} = \frac{\pi}{4} \times 0.05^2 = 0.00196 \text{ m}^2$$

Coeff. of discharge (C_d) = 0.6

$$K = C_d \cdot a \cdot \sqrt{2g} = 0.6 \times 0.00196 \times \sqrt{2 \times 9.81} = 0.0052$$

Inflow (Q_i) = 14 lps = 0.014 m³/s

Initial head (H₁) = 0m

Final head (H₂) = 1.5m

Time required to fill the tank (t) = ?

Water escaped through orifice = ?

$$t = \frac{2A}{K^2} \left[Q_i \ln \frac{Q_i - K\sqrt{H_2}}{Q_i - K\sqrt{H_1}} + K(\sqrt{H_2} - \sqrt{H_1}) \right]$$

$$t = \frac{2 \times 0.2827}{0.0052^2} \left[0.014 \ln \frac{0.014 - 0.0052\sqrt{1.5}}{0.014 - 0.0052\sqrt{0}} + 0.0052(\sqrt{1.5} - \sqrt{0}) \right]$$

t = 44.46 Sec

Inflow volume = $Q_i \times t = 0.014 \times 44.46 = 0.6224 \text{ m}^3$

Volume of water contained in the tank = $A \times H_2 = 0.2827 \times 1.5 = 0.424 \text{ m}^3$

Water escaped through orifice = $0.6224 - 0.424 = 0.1984 \text{ m}^3$

24. A vertical cylindrical tank 2m diameter has, at the bottom, 0.05m diameter sharp-edged orifice ($C_d = 0.6$).

(I) If the water enters the tank at a constant rate of 0.0095 cumecs, find the depth of water above the orifice when the level in the tank becomes stable.

(II) Find the time for the level to fall from 3m to 1m above the orifice when the inflow is turned off.

(III) If water now runs into the tank at 0.02cumecs, the orifice remaining open, find the rate of rise in water level when the level has reached a depth of 1.7m above the orifice.

Solution:

Diameter of tank (D) = 2m

Area of tank (A) = $\frac{\pi}{4} \times 2^2 = 3.14 \text{ m}^2$

Diameter of orifice (d) = 5cm = 0.05m

Area of orifice (a) = $\frac{\pi}{4} \times 0.05^2 = 0.00196 \text{ m}^2$

Coeff. of discharge (C_d) = 0.6

General equation for tank with inflow (Q_i) and outflow (Q_o)

$$(Q_i - Q_o)dt = Adh$$

Where $Q_o = C_d \cdot a \sqrt{2gh} = k\sqrt{h}$ = Discharge through orifice

$$K = C_d \cdot a \sqrt{2g} = 0.6 \times 0.00196 \times \sqrt{2 \times 9.81} = 0.0052$$

I) $Q_i = 0.0095 \text{ m}^3/\text{s}$

Depth of water above orifice (h) = ?

For stable condition, $dh = 0$

$$Q_i = Q_o = K\sqrt{h}$$

$$0.0095 = 0.0052\sqrt{h}$$

$$h = 3.34 \text{ m}$$

II) Initial Head (H_1) = 3m

Final Head (H_2) = 1m

Time required to lower the head from H_1 to H_2 (t) = ?

When the inflow is turned off, $Q_i = 0$

$$(-Q_o)dt = Adh$$

$$dt = -\frac{Adh}{Q_o} = -\frac{Adh}{K\sqrt{h}}$$

$$t = \int_{H_1}^{H_2} -\frac{Adh}{K\sqrt{h}} = \frac{2A}{K}(\sqrt{H_1} - \sqrt{H_2})$$
$$= \frac{2 \times 3.14}{0.0052}(\sqrt{3} - \sqrt{1})$$
$$= 885 \text{Sec}$$

III) $Q_i = 0.2 \text{ m}^3/\text{s}$

Head (h) = 1.7m

Rate of rise in water level (dh/dt) = ?

$$(Q_i - Q_o)dt = Adh$$

$$\frac{dh}{dt} = \frac{Q_i - Q_o}{A} = \frac{Q_i - K\sqrt{h}}{A}$$

$$\frac{dh}{dt} = \frac{0.2 - 0.0052\sqrt{1.7}}{3.14}$$

$$= 0.0615 \text{ m/s}$$

25. A cylindrical tank is placed with its axis vertical and is provided with a circular orifice of 4cm diameter at the bottom. A steady inflow and free discharge at the bottom of the orifice causes the depth of water in the tank to rise from 0.59m to 0.75m in 106 Sec. Further it is observed that the depth rises from 1.2m to 1.29m in 129 Sec. Determine the inflow rate and the diameter of the tank. Assume $C_d = 0.62$.

Solution:

Diameter of orifice (d) = 4cm = 0.04m

Area of orifice (a) = $\frac{\pi}{4} \times 0.04^2 = 0.001257 \text{ m}^2$

Coeff. of discharge (C_d) = 0.62

$$K = C_d \cdot a \sqrt{2g} = 0.62 \times 0.001257 \times \sqrt{2 \times 9.81} = 0.00345$$

Inflow rate (Q_i) = ?

Diameter of tank (D) = ?

First case

$$dh = 0.75 - 0.59 = 0.16 \text{m}$$

$$dt = 107 \text{S}$$

Average head (h) = 0.67m

$$dh/dt = 0.001495$$

Second case

$$dh = 1.29 - 1.2 = 0.09\text{m}$$

$$dt = 129\text{S}$$

$$\text{Average head (h)} = 1.245\text{m}$$

$$dh/dt = 0.000698$$

$$(Q_i - Q_o)dt = Adh$$

$$\frac{dh}{dt} = \frac{Q_i - Q_o}{A} = \frac{Q_i - K\sqrt{h}}{A}$$

Substituting values for both cases

$$0.001495 = \frac{Q_i - 0.00345\sqrt{0.67}}{A}$$

$$Q_i = 0.001495A + 0.002824 \quad (\text{a})$$

$$0.000698 = \frac{Q_i - 0.00345\sqrt{1.245}}{A}$$

$$Q_i = 0.000698A + 0.003849 \quad (\text{b})$$

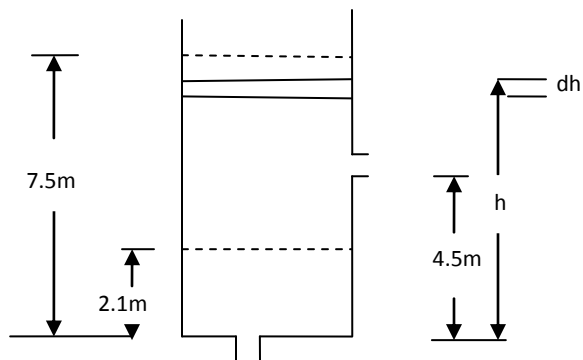
Solving a and b

$$A = 1.285 \text{ m}^2$$

$$Q_i = 0.0047 \text{ m}^3/\text{s}$$

$$D = \sqrt{\frac{4A}{\pi}} = \sqrt{\frac{4 \times 1.285}{\pi}} = 1.28\text{m}$$

26. A tank of constant cross-sectional area of 2.8m^2 has two orifices each $9.3 \times 10^{-4} \text{ m}^2$ in area as shown in the figure. Calculate the time taken to lower the water level from 7.5m to 2.1m above the bottom of the tank. Assume $C_d = 0.62$.



Solution:

$$\text{C/s of tank (A)} = 2.8\text{m}^2$$

$$\text{C/s of orifice (a)} = 9.3 \times 10^{-4} \text{ m}^2$$

Let the water level is at height h above the lower orifice at time t . dh is the decrease in water level in time dt .

Q = discharge

$Qdt = -Adh$

$dt = -Adh/Q$

Discharge from top orifice (Q_1) = $C_d a \sqrt{2g(h - 4.5)}$

Discharge from lower orifice (Q_2) = $C_d a \sqrt{2gh}$

$Q = Q_1 + Q_2 = C_d a \sqrt{2g(h - 4.5)} + C_d a \sqrt{2gh}$

$H_1 = 7.5\text{m}$, $H_2 = 4.5\text{m}$

T_1 = Time taken to lower the water from 7.5m to 4.5m when both orifices are discharging

T_2 = Time taken to lower the water from 4.5m to 2.1m when only lower orifice is discharging

Finding T_1

$$dt = -\frac{Adh}{Q} = -\frac{2.8dh}{C_d a \sqrt{2g(h-4.5)} + C_d a \sqrt{2gh}}$$

$$dt = -\frac{2.8dh}{C_d a \sqrt{2g} [\sqrt{(h-4.5)} + \sqrt{h}]} = -\frac{2.8dh}{0.62 \times 9.3 \times 10^{-4} \sqrt{2g} [\sqrt{(h-4.5)} + \sqrt{h}]}$$

$$dt = -1096.3 \frac{dh}{[\sqrt{(h-4.5)} + \sqrt{h}]}$$

Integrating

$$T_1 = -1096.3 \int_{4.5}^{7.5} \frac{dh}{[\sqrt{(h-4.5)} + \sqrt{h}]}$$

$$T_1 = -1096.3 \int_{4.5}^{7.5} \frac{[\sqrt{(h-4.5)} - \sqrt{h}] dh}{-4.5}$$

$$= 942\text{Sec}$$

Finding T_2 using direct formula

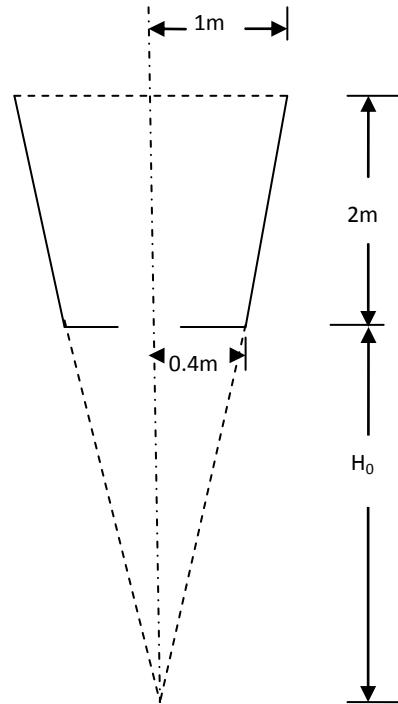
$H_1 = 4.5\text{m}$, $H_2 = 2.1\text{m}$

$$T_2 = \frac{2A}{C_d a \sqrt{2g}} [\sqrt{H_1} - \sqrt{H_2}]$$

$$T_2 = \frac{2 \times 2.8}{0.62 \times 9.3 \times 10^{-4} \sqrt{2g}} [\sqrt{4.5} - \sqrt{2.1}] = 1474 \text{ Sec}$$

Total time taken to empty the tank from 7.5m to 2.1m = $T_1 + T_2 = 2416\text{Sec} = 40.26 \text{ min}$

27. A tank is in the form of frustum of a cone having top diameter of 2m, a bottom diameter of 0.8m and height 2m and is full of water. Find the time of emptying the tank through an orifice 100mm in diameter provided at the bottom. Take $C_d = 0.625$.



Solution:

$$C_d = 0.625$$

$$\text{Area of orifice (a)} = \frac{\pi}{4} \times 0.1^2 = 0.00785 \text{ m}^2$$

$$H_1 = 2\text{m}, H_2 = 0\text{m}, R_1 = 1\text{m}, R_0 = 0.4\text{m}$$

From similar triangles,

$$\frac{1}{2 + H_0} = \frac{0.4}{H_0}$$

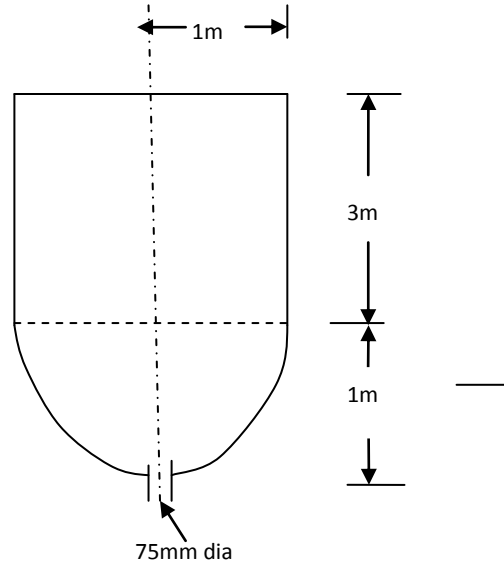
$$H_0 = 1.33\text{m}$$

$$K = \frac{1}{C_d a \sqrt{2g}} \frac{\pi R_1^2}{(H_1 + H_0)^2} = \frac{1}{0.625 \times 0.00785 \sqrt{2 \times 9.81}} \frac{\pi \times 1^2}{(2 + 1.33)^2} = 13.03$$

Time of emptying the tank is

$$\begin{aligned} T &= K \left[\frac{2}{5} (H_1^{5/2} - H_2^{5/2}) + \frac{4}{3} H_0 (H_1^{3/2} - H_2^{3/2}) + 2H_0^2 (H_1^{1/2} - H_2^{1/2}) \right] \\ &= 13.03 \left[\frac{2}{5} (2^{5/2} - 0^{5/2}) + \frac{4}{3} \times 1.33 (2^{3/2} - 0^{3/2}) + 2 \times 1.33^2 (2^{1/2} - 0^{1/2}) \right] = 160 \text{ Sec} \end{aligned}$$

28. A tank is in the form of hemisphere of 2m diameter and having a cylindrical upper part of 2m diameter and 3m height. Find the time of emptying the tank through an orifice of 75mm diameter at its bottom if the tank is initially full of water. Take $C_d = 0.62$.



Solution:

$$C_d = 0.625$$

$$\text{Area of cylinder (A)} = \frac{\pi}{4} \times 2^2 = 3.14 \text{ m}^2$$

$$\text{Area of orifice (a)} = \frac{\pi}{4} \times 0.075^2 = 0.004418 \text{ m}^2$$

T_1 = time taken to lower water from 4m to 1m in the cylindrical part

T_2 = time taken to empty the hemispherical part from 1m to 0m

Computing T_1

$$H_1 = 4\text{m}, H_2 = 1\text{m}$$

$$T_1 = \frac{2A}{C_d a \sqrt{2g}} [\sqrt{H_1} - \sqrt{H_2}]$$

$$T_1 = \frac{2 \times 3.14}{0.62 \times 0.004418 \sqrt{2g}} [\sqrt{4} - \sqrt{1}] = 518 \text{ Sec}$$

Computing T_2

$$H_1 = 1\text{m}, H_2 = 0\text{m}$$

$$T_2 = \frac{\pi}{C_d a \sqrt{2g}} \left[\frac{4R}{3} (H_1^{3/2} - H_2^{3/2}) - \frac{2}{5} (H_1^{5/2} - H_2^{5/2}) \right]$$

$$T_2 = \frac{\pi}{0.62 \times 0.004418 \sqrt{2g}} \left[\frac{4 \times 1}{3} (1^{3/2} - 0) - \frac{2}{5} ((1^{5/2} - 0) - 0) \right] = 242 \text{ Sec}$$

$$\text{Total time taken to empty the tank} = T_1 + T_2 = 518 + 242 = 760 \text{ Sec}$$